

A Wideband Series Fed Patch Array with Side Lobe Level Control

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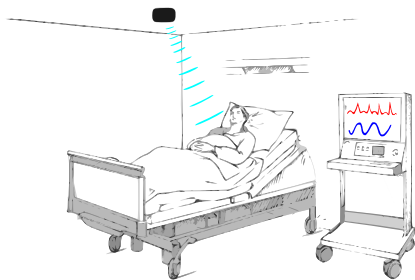


Outline

- 1 Introduction
- 2 Antenna Design and Modelling
- 3 Measurements
- 4 Conclusion

Introduction: Radar technique

Radar systems can perform **non-contact sensing** of cardiorespiratory activity and position. These results are useful for:



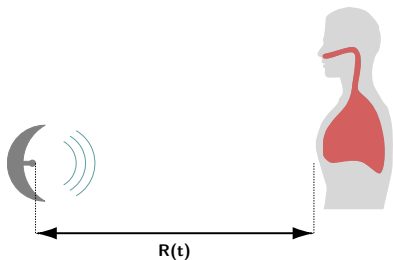
- ▶ monitoring patients with **compromised skin** (burns or chemical contaminations),
- ▶ **home therapy**,
- ▶ **sleep monitoring**,
- ▶ detection of **humans behind walls** or **under rubble**,
- ▶ monitoring people in case of risk of infection or during **pandemics** (e.g. COVID-19 crisis).

Problem Geometry

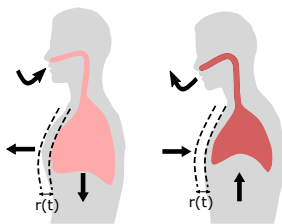
The system must be able to detect information about the subject **position** $\mathbf{R}(t)$ and the **small movements** of his chest $\mathbf{r}(t)$.

$$\mathbf{R}_T(t) = \mathbf{R}(t) + \mathbf{r}(t)$$

Position



Small Movements



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Antenna Design

For radar applications antenna requirements are:

- ▶ **low-cost**
- ▶ **compactness**



**Planar
Antennas**

For a good detection the antenna should exploit the **entire available bandwidth** not to lower the range resolution and to have a **high gain** and **low SLL** to concentrate the main beam on the patient chest and to filter the clutter. Inside the 5.8 GHz ISM band fractional bandwidth is of about 2.6%.

Possible solutions:

▶ **stacked structures**



Complex ✗
Large bandwidth ✓

▶ **hybrid configuration involving series-corporate feed techniques**



Large area occupation ✗
Large bandwidth ✓

▶ **series fed arrays**

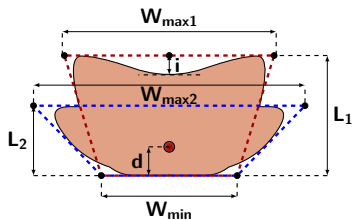


Small bandwidth ✗
Simple and compact ✓

A new **dual band** patch antenna with **side lobe control** has been proposed.

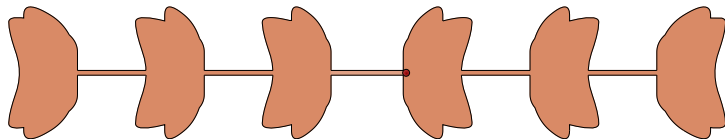
Antenna Design

Antenna Parameters



Parameter	Dimension (mm)
W_{\min}	16.7
$W_{\max 1}$	25
$W_{\max 2}$	30.7
L_1	14.6
L_2	7.15
i	3.6
W_{line}	1
l_{line}	14.34

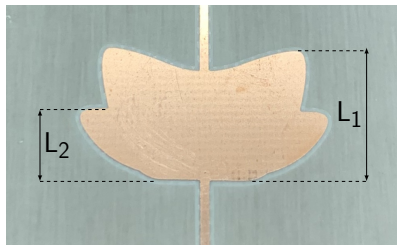
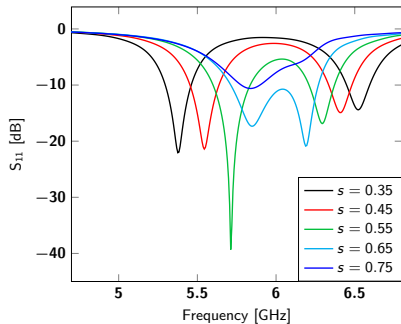
Complete Array



Antenna Design

Bandwidth

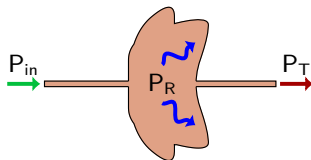
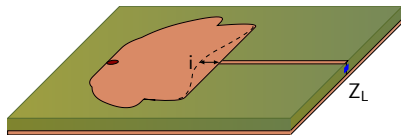
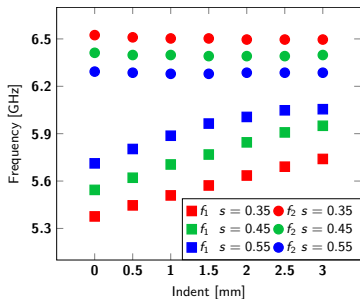
Two resonances are related to the lengths L_1 and L_2 and they can be made closer or more distant by varying the degree of superposition $s = L_2/L_1$.



Antenna Design

SLL Control

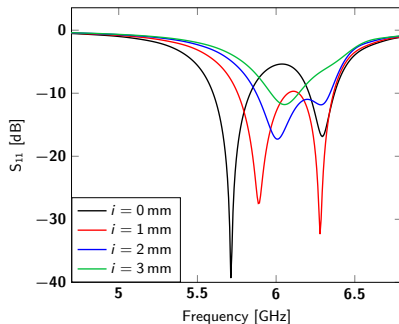
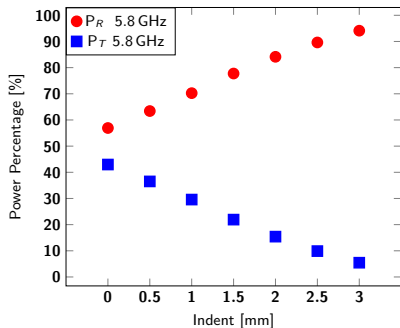
The accepted power at the feeding point of the patch is P_{in} . A portion of this power is radiated (P_R), while the remaining is transmitted to the next elements (P_T). The specific amplitude distribution and correspondingly the side lobe suppression are controlled by the indent degree i .



Antenna Design

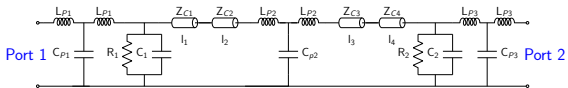
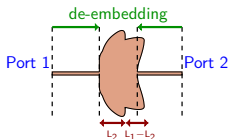
Parameter interaction

The effect of the indent of the upper edge of the patch (i) is not only limited to the control of the side lobe level. If i increases, the overall patch length (L_1) is decreased, with a consequent reduction of the corresponding resonant frequency.

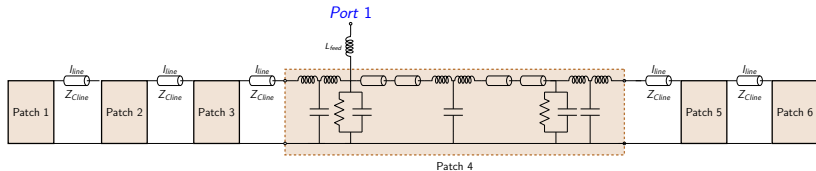
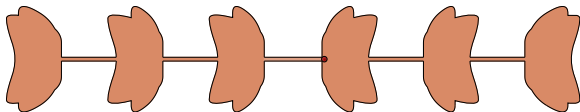


Electrical model

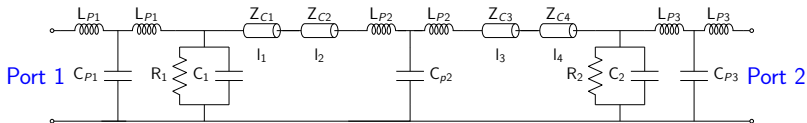
Single patch



Complete Structure

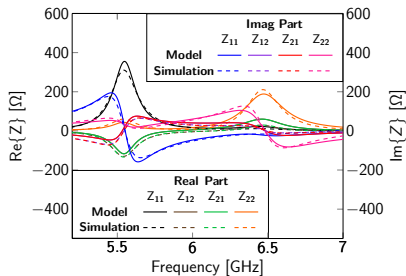


Electrical Model

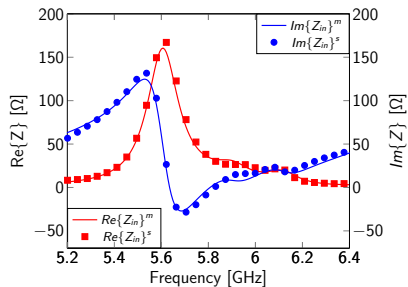


$L_{P1} = 0.16 \text{ pH}$, $C_{P1} = 1 \text{ fF}$, $R_1 = 450 \text{ } \Omega$, $C_1 = 10.01 \text{ fF}$, $Z_{C1} = 13 \text{ } \Omega$, $l_1 = 56.13 \text{ deg}$, $Z_{C2} = 6.50 \text{ } \Omega$, $l_2 = 60.13 \text{ deg}$, $C_{P2} = 39.37 \text{ pF}$, $L_{P2} = 8.00 \text{ pH}$, $Z_{C3} = 14.50 \text{ } \Omega$, $l_3 = 25.72 \text{ deg}$, $Z_{C4} = 7 \text{ } \Omega$, $l_4 = 24.42 \text{ deg}$, $R_2 = 165.10 \text{ } \Omega$, $C_2 = 0.70 \text{ pF}$, $L_{P3} = 0.17 \text{ nH}$ and $C_{P3} = 30.59 \text{ pF}$.

Single Patch



6 Patch Array



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Anechoic Chamber Set-Up

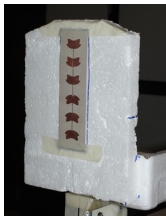
Set-up



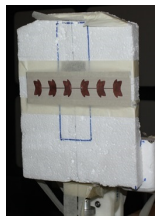
Measuring Antenna: ETS-Lindgren's Model 3117 Double-ridged Waveguide antenna 0 GHz – 18 GHz range

Distance: 2.58 m ($2D^2/\lambda = 0.88$ m at 5.875 GHz)

Dielectric easel for H-plane measurements

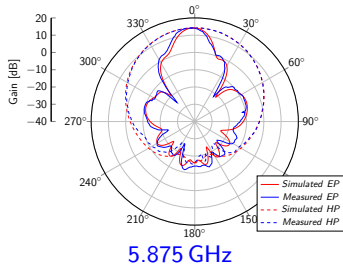
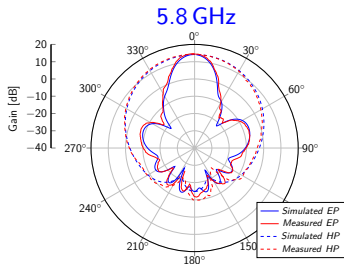
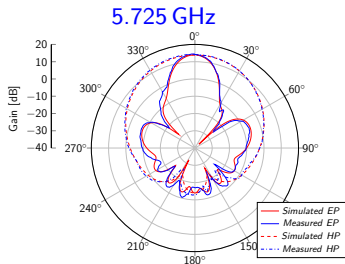


Dielectric easel for E-plane measurements



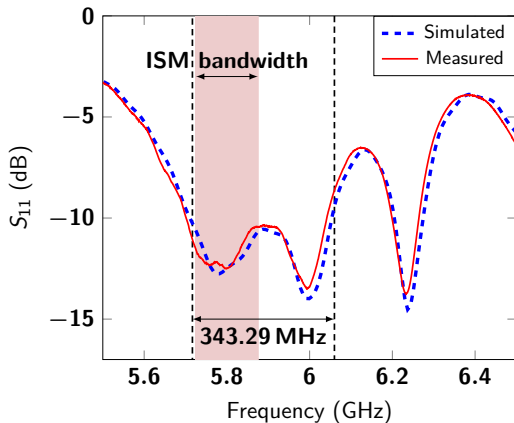
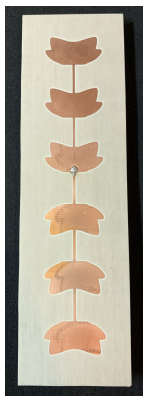
Measurement Results

Radiation Pattern



Measurement Results

Reflection Coefficient



The deigned antenna has a **fractional bandwidth** of about **5.92 %**.

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Conclusions

- ▶ A new patch geometry has been proposed to overcome the limitations of the conventional patch arrays:
 - a dual band structure with overlapping bands can assure a bandwidth enhancement;
 - the indent of the patch upper edge allows the control of the side lobe level and. With this technique a low SLL is assured with patches with the same shape.
- ▶ The designed antennas have been realised and measured, showing an excellent agreement between measurements and simulations, both for the scattering parameters and the radiation pattern.