Electrostatic Doping Assisted Push-Pull Mach-Zehnder Modulator For Optical Interconnects

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Why Silicon Photonics?



Problems in Present Design

- Fixed bandwidth capability.
- High power consumption.
- Scaling limitation.

Solution(s)

- Replacement of copper based interconnects by photonic interconnects.
- Integration of electronic and photonic circuits.



Why Silicon Photonics?

Advantages of Silicon

- Stable and well understood material.
- Mature fabrication technology.
- High optical confinement and refractive index.
- Optically transparent at 1.3 μ m to1.5 μ m.
- Electro-refraction and electro-absorption: dual method for optical modulation.
- Offers electronic and optical integration.

Requirements of Silicon Based Interconnects

- Power Requirement¹: Inter-chip: $\leq 100 \text{ fJ/bit}$; Intra-chip: $\leq 50-200 \text{ fJ/bit}$.
- Photodetectors integrated with transistors.
- Total time delay: 180-270 ps.
- Total power consumption: 18-20 mW.





Optical Modulators in Photonic Integrated Circuits

Optical Phase Shifters and Modulators

- Phase shifter introduces additional phase shift in guided-light.
- Additional phase shift: $\Delta \phi = (2\pi L \Delta n) / \lambda$
- Δn : Electro-optic effect (via free carrier plasma dispersion effect) or thermo-optic effect.
- Most common structure: PN/PIN diode or MOS Capacitor in a rib waveguide.

Different Modulator Structures



Different Optical Modulator Structures



Random Dopant Fluctuations



Source: Roy et al., Science Magazine, vol. 309, pp.388-389, July 2005.

Source: Gabriele Tocci, Masters Thesis, KTH, 2010.

Source: L. Gerrer et al., Microelectronics Reliability, vol. 52, pp. 1918-1923, 2012.

Insertion loss in MZM as a function of doping¹: I

$$: \left| \text{IL} = 2\alpha_{sp} + \left(A \cdot \sqrt{N_{dop}} + \frac{\alpha_{wg}}{\sqrt{N_{dop}}} \right) \cdot B \right|$$

where α_{sp} : splitter loss; *A*, *B*: two coefficients related to length and light overlap factor; N_{dop} : doping concentration; and α_{wg} : optical propagation loss.

¹ Xi Xiao et.al., *Optics Express*, vol. 21, no. 4, pp. 4416-4125, 2013.

Origin of Random Dopant Fluctuations



Plausible Solution?

Use of Electrostatic Doping (ED)



Concept of Electrostatic Doping (ED)



Figure: Concept of ED in metal-semiconductor and metal-insulator-semiconductor junction.

Types of ED in Semiconductor Devices

- Schottky Barrier Based Doping SB-MOSFET, SB-FinFET, CNT
- Work-function Induced Doping CP-PN/PIN diode, CP-BJT, CP-TFET

Bias Induced Doping

Lateral/ vertical PN junction, DG-TFET

Plausible ED in Si-Ph Devices

- Work-function induced doping Utilizes different metal as electrodes.
- Bias induced doping

Use of proper bias voltages.

Design Objectives

• ED assisted optical phase shifter based Push-Pull Mach-Zehnder Modulator (MZM).



Proposed ED Assisted Push-Pull MZM

Proposed Modulator Structure





Carrier Distribution Across ED Assisted Optical Phase Shifter





 $10^{10.1}$

10^{16.1}

 $10^{5.35}$

Mathematical Model of Proposed Modulator

Referring to the device structure, the output electric field of the modulated signal (E_{out}) can be expressed as:

$$E_{out} = \left[\sqrt{\gamma_1 \gamma_2} e^{-j\Delta\phi(v_1)} e^{-\Delta\alpha(v_1)L}\right] e^{-(j\phi_0 + \alpha_0 L)} E_{in} + \left[\sqrt{(1 - \gamma_1)(1 - \gamma_2)} e^{-j\Delta\phi(v_2)} e^{-\Delta\alpha(v_2)L}\right] e^{-(j\phi_0 + \alpha_0 L)} E_{in}$$

For symmetric power splitting and combining i.e. $\gamma_1 = \gamma_2 = \frac{1}{2}$, the above equation reforms to:

$$E_{out} = \frac{E_{in}}{2} \left[e^{-j\Delta\phi(v_1)} e^{-\Delta\alpha(v_1)L} + e^{-j\Delta\phi(v_2)} e^{-\Delta\alpha(v_2)L} \right] e^{-(j\phi_0 + \alpha_0 L)}$$

where, $\Delta \phi(v) = \frac{2\pi L}{\lambda} \Delta n(v)$: bias voltage induced phase change in the optical phase shifter $\lambda = \text{operating wavelength};$ $\phi_0 = \text{phase shift at zero bias voltage};$ $\alpha_0 = \text{loss coefficient at zero bias voltage};$ L = length of the phase shifter.

Simulation Setup for the Proposed Modulator



Used Simulation Platform

Carrier Dynamics: Lumerical Device CT Modal Calculation: Lumerical Mode Solutions Transmission System: Lumerical Interconnect



Simulation Results: Dynamic Performance Metrics



Performance Metrics: Design 1

L = 200 μm 3-dB EO Bandwidth: 28 GHz Maximum operating frequency: 35.2 GHz

Performance Metrics: Design 2

 $L = 400 \ \mu m$

3-dB EO Bandwidth: 22.7 GHz

Maximum operating frequency: 30.3 GHz



Simulation Results: Eye Diagram After Different Fiber Length at 10 Gb/s Data Rate



Fiber Length (km)	Dynamic ER (dB)
B2B	5.93
0.5	5.26
1.0	4.68
5.0	3.64

Transient Performance Metrics

 $L=200\;\mu m$

3-dB EO Bandwidth: 28 GHz

Maximum operating frequency: 35.2 GHz



Simulation Results: BER Performance



Simulation Parameters

Data Rate: 25 Gb/s Input Data: 2¹¹-1, PRBS Thermal Noise: -410 dBm/Hz Dark Current: 5 nA Responsivity: 0.85 A/W



Comparative Performance Study

Reference	Year	Material	L [mm]	ER [dB]	IL [dB]	f _{max} [GHz]	$V_{\pi}L_{\pi}$ [V.cm]
[10]	2019	Si	3	3.6	9.1	32	0.55
[11]	2019	Si-LiNbO ₃	3	5.0	2.5	112	2.20
[19]	2019	AlGaAs	10	3.0	7.5	-	1.00
This work	2020	Si	0.2	4.7	5.1	30.3	0.36-0.74

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Conclusions

- Push-Pull Mach-Zehnder intensity modulator with electrostatic doping assisted optical phase shifter for photonic integrated circuits is plausible.
- For 200 μ m long proposed MZM, estimated dynamic ER is 4.7 dB with 5.1 dB of IL at 10 Gb/s data rate.
- 3-dB electro-optic bandwidth of MZM with $L = 200 \ \mu m$: 28 GHz.
- Maximum operating frequency of MZM with $L = 200 \ \mu m$: 35.2 GHz.
- Transmission over 5 km SSMF fiber also plausible.
- Power penalty at 25 Gb/s data rate over 1 km and 5 km SSMF: 5 dB and 13 dB, respectively.



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Thank You